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through mud-pulse or electromagnetic-wave telemetry. While MWD operations are possible [[much]] most of the time, manual measurements are often desired either for verification purposes[[,]] or the measurements desired are not within the capabilities of the MWD system currently in the wellbore. Whatever the reason, it is desirable to maintain the differential in bore and annulus pressure downhole so that mud motors or other downhole equipment may continue to function while the operation is performed. Typically, the measurements are made by engaging a "tool" connected to a communications "conduit" within the bore of the drillstring and deploying the tool to the desired depth.

Please replace paragraph [0006] with the following amended paragraph:

[0006] For the purposes of this disclosure, the term "tool" is very generic and may be applied to any device sent downhole to perform any operation. Particularly, a downhole tool can be used to describe a variety of devices and implements to perform a measurement, service, or task, including, but not limited to, pipe recovery, formation evaluation, directional measurement, and workover. Furthermore, the term "conduit," while frequently thought of as a tubular member for housing electrical wires, in oilfield parlance[[,]] is used to describe anything capable of transmitting hydraulic, electrical, mechanical, or light communications from one location (surface) to another (downhole). For this reason, the term conduit[[,]] as applied with respect to the present disclosure is to include electrical or mechanical wireline, slick line, coiled tubing, fiber optic cable, and any present or future equivalents thereof.

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Please replace paragraph [0007] with the following amended paragraph:

[0007] Historically, the deployment of tools on a communications conduit to the bore of a drillstring has been accomplished through the use of entry subs. Entry subs, in their simplest form, include two inlets and a single outlet. Fluid (drilling mud) enters through one inlet under pressure, a communications conduit is manipulated through the second inlet, or entry port, and both the conduit and the pressurized fluid exit through the single outlet. The development of entry subs over the years has yielded various improvements to oilfield technology, but has identified numerous needs as well.

Please replace paragraph [0008] with the following amended paragraph:

[0008] Drillstring pipe sections are preferably mounted below the entry sub at the outlet and above the sub at the fluid inlet. Frequently, entry subs are used in combination with top-drive assemblies to enable tools and the conduit attached thereto to be engaged within the bore of the drillstring while the drillstring is being rotated. With a rotational swivel located between the entry sub and the rotary table of the rig floor, the top-drive assembly is used to raise, lower, and hold the entry sub rotationally still from above while the rotary table rotates the drillstring below. This combination allows the drillstring to be rotated (and prevented from becoming stuck) while the tool disposed on the communications conduit is deployed into the bore of the drillstring. Because the entry sub provides a sealing engagement with respect to the conduit entering therethrough, drilling mud can be continued to be maintained at pressure while the conduit is deployed.

Please replace paragraph [0010] with the following amended paragraph:

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[0010] This arrangement required the conduit and any tool attached thereto to overcome an angle of inclination in order to pass through the tool body en route to the lower pipe section. For this reason, only the smallest and most flexible of tools (and conduits) were capable of being used with the side entry sub, severely limiting the benefits of using the device. Larger, more rigid, tools required the bottom drillstring connection to be separated (preventing the maintenance of drilling fluid bore pressure) while the tools were "made up" and inserted into the bore of the drillstring. These tools would be connected to the conduit (previously stripped through the side entry port) and run partially into the drillstring before the connection between the side entry sub and the drillstring (as well as the drilling fluid pressure) could be restored. These operations required a lengthy break in mud flow operations that could be costly in terms of rig time, ~~as well as in terms of when used, would need to be made up below the bottom tool joint of the entry sub and would be stripped into the drillstring without being able to maintain fluid pressure.~~

Please replace paragraph [0012] with the following amended paragraph:

[0012] However, another primary function of the top entry sub (as a member of the drillstring) is to support the total weight of the complete length of the drillstring. To manipulate the drillstring up and down into the well, the top-drive assembly (or derrick crane lifting block) must be capable of lifting several thousand feet of steel drill pipe at one time. While the drilling fluid serves to buoy some of this total weight, lengthy drillstrings frequently weigh hundreds of thousands of pounds, depending on their length, diameter, and sidewall thickness. As an integral component of the drillstring when installed, the top entry sub must

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also be capable of supporting loads of this type. However, much concern arose with the loading capabilities of the top entry sub because of the axial offset between the bottom drillstring connection and the top drillstring connection. This offset, while allowing a conduit and tools attached thereto to be engaged straight into the drillstring without overcoming a bend angle, [[also]] could potentially induce bending moments and loads in the body of the top entry sub[[,]] if high tensile loads were applied across drillstring inlet and drillstring outlet ports.

Please replace paragraph [0013] with the following amended paragraph:

[0013] As a result of these concerns, investigations were performed to determine the bending moments experienced across the top entry sub and within the rotary threaded connections for the drillstring components attached thereto. While the results indicate that the bending loads and moments are not a significant factor, there is still the perception by some in the industry that the loads remain a factor. Additionally, as drilling technology progresses, deeper and smaller diameter wells are being drilled everyday, particularly offshore in deep water situations. Therefore, the offset nature of the top entry sub may again become an issue in that deeper wells require longer lengths of pipe, resulting in even higher tensile loads. Furthermore, the smaller "gauge" drillstring that may be employed would require a similarly gauged top entry sub, one that may not, if produced, be capable of carrying the higher tensile loads without incurring the problems associated with bending moments. An entry sub arrangement capable of both allowing tools disposed upon a communications conduit to be engaged into the bore of a drillstring and handling extreme tensile drillstring loads would be highly desirable.

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Please add the following new paragraph after paragraph [0015]:

[0015.1] In another embodiment, an entry sub includes a tubular member with opposed articulating joints at respective first and second ends thereof, a first longitudinal passage in the tubular member opening at the joint at the first end, a second longitudinal passage in the tubular member diverging from the first longitudinal passage and in communication between the first longitudinal passage and the joint at the second end, and a third longitudinal passage in the tubular member in communication between the first longitudinal passage and a port in the second end of the tubular member. In yet another embodiment, an articulated top entry sub includes a tubular member, a first longitudinal bore into the member from a lower drillstring port at a lower end, a second longitudinal bore into the member from a wireline entry port at an upper end to communicate with the first longitudinal bore, a third longitudinal bore from an upper drillstring port at the upper end to communicate with the first longitudinal bore at a divergent angle, an upper drillstring connection sub having a lower end terminating at an upper deflection joint in the upper drillstring port having a maximum deflection angle at least as great as the divergent angle, and a lower drillstring connection sub having an upper end terminating at a lower deflection joint in the lower drillstring port having a maximum deflection angle at least as great as the divergent angle. In another embodiment, the joints can include a sleeve formed in each respective drillstring port having an annular posterior shoulder with an outside diameter greater than the respective bore, a convex rotational surface at an enlarged terminus of the drillstring connection having a diameter less than the sleeve and greater than the bore, a posterior annular seat between the terminus and the shoulder comprising a matching concave rotational surface, an anterior annular seat having an outside diameter to be received in the sleeve, a matching inside

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concave rotational surface, and an inside diameter greater than an outside diameter of a longitudinal section of the respective drillstring connection sub, and a retention nut threadably received in the sleeve to secure the annular seats and having an inside diameter larger than the outside diameter of the longitudinal section.

Please replace paragraph [0016] with the following amended paragraph:

[0016] The deficiencies of the prior art can also be addressed by a method to deploy tools connected to a distal end of a communications conduit into a drillstring by connecting an articulatable entry sub to the drillstring, wherein the entry sub provides an entry port, upper and lower connections to the drillstring, and an articulated knuckle joint. Preferably, the entry port is connected to the lower connection of the drillstring by a communications pathway. The method preferably includes articulating the entry sub so the communications pathway and the lower connection to the drillstring are substantially coaxial. The method preferably includes engaging tools through the entry port, the communications pathway, the lower connection to the drillstring, and into a portion of the drillstring located below the entry sub. The method preferably includes articulating the entry sub so the communications pathway is axially skewed from the lower connection to the drillstring. In another embodiment, a wireline service method for a drill string including a top drive and a rotary table includes installing a top entry sub with opposing deflection knuckles into the drill string above the rotary table and below the top drive, positioning the deflection knuckles to align an entry port of the top entry sub with the drill string below the top entry sub and offset the drill string above the top entry sub, inserting a wireline tool suspended from a wireline through the aligned entry port into the drill string below the entry sub, positioning

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the deflection knuckles to align the drill string above and below the entry sub and offset the entry port, and operating the tool in the drill string below the entry sub with the wireline through the entry port.

Please replace paragraph [0023] with the following amended paragraph:

[0023] Referring initially to FIG. 1, a profile-view drawing of an entry sub system 10 having two articulated knuckle joints 30, 32 is shown. Entry sub system 10 includes an entry sub body 12 having an upper end 14 and a lower end 16. Sub body 12 may be constructed as a tubular body or any other structurally sound configuration. An upper section of pipe 18 extends up from upper knuckle joint 30 at upper end 14 and a lower section of pipe 20 extends from lower knuckle joint 32 at lower end 16. Pipe sections 18 and 20 each include rotary threaded drillstring connections 22, and [[14]] 24 respectively. Threaded drillstring connections Connections 22 and 24 are commonly referred to in the art as "tool joints," in that they allow for the connection of additional oilfield tools or drillstring components thereto. Threaded drillstring connections Connections 22, 24 can be of any rotary threaded tool joint connections as one skilled in the oilfield arts would have available, but are preferably standard American Petroleum Institute (API) designs. Preferably, threaded drillstring connections 22, 24 are sized and specified so as to match corresponding tool joints of adjacent drillstring components (not shown).

Please replace paragraph [0024] with the following amended paragraph:

[0024] Entry sub system 10 is preferably installed above a wellhead with the remainder of the drillstring (not shown) mounted below at connection 24 and above at connection 22. While installed in a drillstring, entry sub system 10 allows

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for the transfer of drillstring fluids and loads therethrough, all the while providing for the entry of tools into the drillstring through an entry port 26 (more easily viewed in sectioned FIG. 2). Using entry sub system 10, a drilling operator is able to maintain drilling fluids in the bore of the drillstring at pressure while allowing tools inserted into the pressurized bore through entry port 26 to perform oilfield operations below. Tools inserted through entry port 26 ~~will~~ can be of numerous functions and types and will typically be deployed upon the distal end of a communications conduit. Entry port 26 of sub body 12 is preferably sized and constructed so that as many tools as possible are able to pass therethrough, into lower pipe section 20, and further downhole. Entry port Port 26 is preferably constructed so that lower knuckle joint 32 can be manipulated so that the center axis of lower pipe section 20 is substantially coaxial to the center axis of entry port 26, thereby allowing passage of tools and communications conduit therethrough with little or no obstruction.

Please replace paragraph [0025] with the following amended paragraph:

[0025] Referring now to FIG. 2, a cross-sectional profile view of the entry sub system 10 is shown. As can now be seen more clearly, sub body 12 includes a conduit entry passage 40, a fluid inlet passage 42, and a fluid and conduit exit passage 44. A communications conduit 5 is shown entering sub body 12 at entry port 26, extending through conduit entry passage 40 until it reaches fluid and conduit exit passage 44 where it proceeds with fluid flow from fluid inlet passage 42 through lower knuckle joint 32 into lower pipe section 20. Preferably, a hydraulic pack off device (not shown), known to one skilled in the art, is located at a receptacle 46 at the beginning of conduit entry passage 40 at entry port 26 to prevent hydraulic fluid[[s]] from passages 40, 42, and 44 from escaping entry sub

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system 10 around communications conduit 5 or when communications conduit 5 is absent.

Please replace paragraph [0026] with the following amended paragraph:

[0026] Optionally, a receiving profile 48 can be located within conduit entry passage 40 along the length of sub body 10 12 where communications conduit 5 would be expected to contact and abrade the wall of conduit entry passage 40. Receiving profile Profile 48 may be of any type and design to either prevent abrasion of passages 40 [[of]] and 44 resulting from extended manipulation of communications conduit 5 therethrough. One example for receiving profile 48 would include a build-up of hardened, wear-resistant, material such that life of sub body [[10]] 12 is maximized. Alternatively, receiving profile 48 can be constructed as a replaceable sleeve of hardened material that could be replaced when worn.

Please replace paragraph [0027] with the following amended paragraph:

[0027] As communications conduit 5 passes through fluid and conduit exit passage 44, lower knuckle joint 32 is encountered. Knuckle joints 30[[,]] and 32 are preferably constructed as ball-and-socket joints but any flexible joint (including, but not limited to, a U-joint design) known to one skilled in the art may be employed. Knuckle joints are shown located within receptacles 50, 52 of sub body 12 and are designed to receive substantially spherical ends 54, 56 of pipe sections 18 and 20, respectively. Furthermore, knuckle joints 30, 32 may also be constructed to either restrict or allow relative rotational movement between sub body 12 and pipe sections 18, 20. By adding splines (or their mechanical

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equivalent) to substantially spherical ends 54, 56, they can be prevented from rotating with respect to their receptacles 50, 52 in sub body 12.

Please replace paragraph [0028] with the following amended paragraph:

[0028] To receive substantially spherical ends 54, 56, spherical sockets 58 are placed within receptacles 50 and 52. Spherical sockets Sockets 58 may be constructed of any material known in the art, but are preferred to be manufactured of high-strength and wear-resistant materials to maximize their longevity. Furthermore, sealing methods known in the art may be easily employed to prevent fluid[[s]] from passages 40, 42, and 44 from escaping through any interfaces between spherical sockets 58 and receptacles 50, 52 or between spherical sockets 58 and substantially spherical ends 54, 56. Metal-to-metal seals, elastomeric seals, and fiber-reinforced polymer seals can be so employed. If substantially spherical end 54, 56 to sub body rotation is desired, the seals must be capable of experiencing the rotation without a loss in performance.

Please replace paragraph [0029] with the following amended paragraph:

[0029] Following installation of spherical socket 58 into receptacle 50, 52, substantially spherical ends 54, 56 are engaged therein, and ~~backup~~ compression rings 60 are installed. Compression rings 60 may also be of any material known in the art but are also preferred to have high compressive strength and good wear resistance. Furthermore, to ease in their installation, compression rings 60 may be segmented (for instance, in halves) so the outside diameters of pipe sections 18, 20 may be larger than the internal diameters of compression rings 60. Finally,

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compression nuts 62 are installed behind compression rings 60 and tightened to compress knuckle joints 30, 32 together and properly seat any seals therein.

Please replace paragraph [0030] with the following amended paragraph:

[0030] Additionally, a replaceable abrasion sleeve 64 may be installed within substantially spherical end 56 of lower knuckle joint 32 to protect the material of lower pipe section 20 from abrasion from continued manipulation of communications conduit 5 therethrough. Abrasion sleeve 64 is preferably constructed of a hardened metal but may also be constructed as a relatively soft material with an applied hardness coating to increase wear resistance thereof. Finally, a hardened sleeve or hardened coating may optionally be applied to inner diameter 66 of lower pipe section 20 to resist any wearing experienced thereof from communications conduit 5.

Please replace paragraph [0031] with the following amended paragraph:

[0031] Referring briefly to upper knuckle joint 30, no hardened wear sleeve is shown. Instead, substantially spherical end 54 includes a conical profile 68 that allows fluid flowing therethrough to pass more easily. Because no communications conduit 5 is expected to pass through upper knuckle joint 30, a hardened wear sleeve (similar to item 64) is not needed, but may, nonetheless, be used. Optionally, upper pipe section 18 can be constructed similarly to lower pipe section 20 below in the event that lower pipe section 20, or its components, becomes worn and no replacement is immediately available. If components of lower pipe section 20 become worn, it can be swapped with upper pipe section 18, allowing operations to continue while replacements are located.

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Please replace paragraph [0032] with the following amended paragraph:

[0032] FIG. 2 shows entry sub system 10 experiencing a tensile load condition, one where the central axis of pipe sections 18 and 20 are substantially coaxial, in contrast to FIG. 1 where entry port 26 and lower pipe section 20 are substantially coaxial. This condition occurs when large tensile loads (for example, when the drillstring is lifted or maintained in tension by the top-drive assembly or traveling block of the oil derrick) are placed across sub body 12 through pipe sections 18 and 20. Knuckle joints 30, 32 are constructed to be capable of carrying significant tensile loads without hazard. In the position shown in FIG. 2, knuckle joints 30, 32 allow sub body 12 to be cocked to the side and thereby prevent any bending moments from building up therein. As such, the tensile forces from below are carried through lower knuckle joint 32, sub body 12, and up through upper knuckle joint 30 to the traveling block and/or top-drive assembly coaxially without placing any drilling components in any bending conditions.

Please replace paragraph [0033] with the following amended paragraph:

[0033] In [[this]] the configuration shown in FIG. 2, entry port 26 permits communication of communications conduit 5 and any tools attached thereto through lower knuckle joint 32, lower pipe section 20, and into the remainder of the drillstring, but the amount of clearance is diminished by the angular displacement between entry port 26 and lower pipe section 20. This diminished amount of clearance may prevent the largest and most inflexible tools from being able to pass through lower knuckle joint 32, fluid and conduit exit passage 44, and conduit entry passage 40, but many useful tools will still be able to pass. When

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larger clearance from entry port 26 through to lower pipe section 20 and drillstring connected thereto is needed, the axial drillstring loading can be temporarily reduced (for example, by setting slips below), thereby allowing the conduit entry passage 40 and lower pipe section 20 to once again line up in a substantially coaxial arrangement, allowing tools and conduit to be easily engaged or removed therethrough. Once the tool or conduit is removed or inserted, the drillstring loading can be re-applied, allowing knuckle joints 30, 32 to tilt sub body 12 again. While a reduced clearance for communications conduit 5 and tools exists in the position shown in FIG. 2, there still remains enough clearance for manipulation of the conduit in and out of the wellbore.

Please replace paragraph [0035] with the following amended paragraph:

[0035] Referring briefly to FIGS. 3 and 4 together, an alternate embodiment of the entry sub system 100 is shown. Entry sub system 100 is configured to allow an existing top entry sub 112 (or in some instances, a side entry sub) without knuckle joints to be converted for knuckle joint use. Particularly, entry sub system 100 includes an upper knuckle adapter 118 and a lower knuckle adapter 120. Upper knuckle adapter 118 is attached to a drillstring inlet located at an upper end 114 of existing top entry sub 112 while lower knuckle adapter 120 is attached to a drillstring outlet located at a lower end 116 of existing top entry sub 112. Each knuckle adapter 118, 120 would likewise provide a corresponding knuckle joint 130, 132 and a subsequent connection to the drillstring 122,124. The ability to convert prior entry subs for knuckle joint use avoids scrapping potentially outdated technology (cost savings) and allows a rigsite operator to customize his or her entry sub solution according to their particular needs (customer choice).